

## ISOTHERM STUDIES OF EQUILIBRIUM SORPTION OF Fe(III) ONTO UNMODIFIED HEN EGGSHELL ADSORBENT

**Dr. Yogesh C. Rotliwala<sup>1</sup>, Mikesh H. Chevli<sup>2</sup>, Neha Maheshwari<sup>3</sup>**

Head, Chemical Engineering, SNPIT & RC, Bardoli, Gujarat, India <sup>1</sup>

Assistant Professor, Chemical Engineering SNPIT & RC, Bardoli, Gujarat, India <sup>2</sup>

Student, Energy & Environment, Symbiosis Institute of International Business, Pune,  
Maharashtra <sup>3</sup>

*Abstract: The paper explores the study of equilibrium isotherms and potentiality of untreated hen egg shell as a bio waste sorbent for the removal of Fe (III) from aqueous solution. The adsorption data were fitted to different Isotherm models. Regression coefficient ( $R^2$ ) for different models was calculated and observed to be in the order of Langmuir > Freundlich > Temkin > Dubinin–Radushkevich. Favourable adsorption was analysed by determining separation factor ( $R_L=0.136$ ) in a Langmuir isotherm and cross verified by adsorption intensity ( $n=1.61$ ) in a Freundlich isotherm. Moreover, physical adsorption was confirmed with the apparent energy of adsorption (1.0 kJ/mol) in a Dubinin-Radushkevich isotherm model and heat of adsorption (8.239 J/mol) from Temkin isotherm model. Study shows that untreated hen egg shell can be utilised as a bio waste sorbent for the removal of Fe (III) from aqueous solution.*

**Keywords:** Equilibrium adsorption modelling, Heavy metals, Hen egg shell, Isotherm, Sorption

### I. INTRODUCTION

Due to industrialization in last two decades, there has been growing concern over the diverse effects of heavy metals bearing waste water on humans and aquatic ecosystems [1]. Major source of heavy metal bearing waste water mainly includes steel industries, aeronautic, metal coating, etc and requires costlier treatment, e.g. ion exchange, biodegradation, oxidation, solvent extraction and adsorption [2, 3]. Recently, adsorption technique (with the use of waste solids) for the removal of heavy metals from the effluent is reported effective due to low cost, ease of handling and less chemical consumption. Moreover, resource recovery potential for the value added metal can be exploited [4, 5].

Food processing, egg breaking and hatching industries are the major source of egg shell waste (11 % of egg weight), which are available in huge quantities. About 2,50,000 tons of egg shell waste is produced annually worldwide by the food processing industry only. Most of the eggshell waste is commonly discarded of in landfills without any pretreatment because it is traditionally useless and ultimately creates serious environmental problems [6]. The chemical composition of egg shell (94% calcium

carbonate, 1% magnesium carbonate, 1% calcium phosphate and 4% organic material), as well as the porous nature of egg shell structure (7000-17000 pores) [7] leading to serve as attractive material as an adsorbent. Recovery and utilization of calcium in egg shell for the production of cellulose is reported [6]. Chicken egg shell membrane accounted to be effective low cost adsorbent for the removal of anion and cation dyes [8]. Many authors have developed costlier method for the removal of iron from waste water with the use of duck and crab egg shell [9, 10, 11].

The present work addresses the study for effect of adsorbent (eggshell) and adsorbate (stock solution) on the adsorption efficiency of Fe(III) from synthetic aqueous solution by hen eggshell. Besides, the present study is also aimed to evaluate the equilibrium of adsorption process using Langmuir, Freundlich, Temkin and Dubinin–Radushkevich (D – R) Isotherms.

## II. MATERIALS AND METHODS

### A. Preparation of Eggshell

The hen eggshell used in this study was obtained from local food stall located in the city of Surat, India. The eggshell was washed with distilled water several times to remove surface impurities, sundried followed by oven dried at 105 °C for 2 hours. The dried eggshell was grounded using pestle and mortar and the particle size was adjusted in the range of 125-500 μm to increase the surface area for efficient adsorption. Physico-chemical properties of hen eggshell are shown in Table 1.

**TABLE 1:- PHYSICO-CHEMICAL CHARACTERISTICS OF HEN EGGSHELL**

Surface Area	7.0 m <sup>2</sup> /g	Saers Method (Reference 12)
pH	8.1-8.9	IS 3025 (Part 11) (1983, Reaffirmed 2002)
Moisture	8 %	ASTM D5142- 02a
Particle Size	125-500 μm	Using Sieve Analysis
Bulk Density	1.346 g/cm <sup>3</sup>	S. Toshiguki et al. (Reference 13)

### B. Preparation of Adsorbate

The adsorbate was prepared by synthesizing standard stock solution of Fe(III) by dissolving in distilled water. All chemical used in the present study were of analytical grade from Fisher Scientific, India. Atomic Absorption Spectrophotometer (AAS Model A 303, Thermo Scientific) was used to measure the Fe(III) concentration.

### C. Experimental

Series of solutions containing different initial concentrations of Fe(III) ions (in the range of 5-50 mg/L) was prepared and employed for the batch adsorption studies at 30°C to check the applicability of the Langmuir, Freundlich, Temkin and Dubinin– Radushkevich (D – R) adsorption isotherms under optimum conditions (120 minutes on the magnetic stirrer at constant revolution in the pH range between 6 to 6.5). The mixture was centrifuged and the iron concentration was determined using Atomic Absorption Spectrophotometer (AAS Model A 303, Thermo Scientific). As shown in Table 2 the amount of solute adsorbed and the removal efficiency was calculated with the use of reported mass balance equations [14].

$$Q = \frac{V(C_i - C_e)}{M} \dots\dots\dots (1)$$

$$E = \frac{(C_i - C_e)}{C_i} \times 100 \dots\dots\dots (2)$$

Where, Q is the amount of solute adsorbed from the solution (mg/L). V is the volume of the adsorbate (L), C<sub>i</sub> is the concentration before adsorption (mg/L), C<sub>f</sub> is the concentration after adsorption (mg/L), M is the mass of eggshell used (g) and E is the percent removal efficiency.

### III. RESULTS AND DISCUSSION

#### A. LANGMUIR ADSORPTION MODEL

Monolayer adsorption process is described quantitatively by Langmuir adsorption model. The model assumes uniform contact between the surface of adsorbate and adsorbent and that; there should be specific number of adsorption sites on the surface of the adsorbent onto which the solute molecules can be adsorbed [15]. Further, the energy of adsorption onto the surface should be uniform and there should be no transmigration of adsorbate in the plane of the surface [16]. Based upon these assumptions, the Langmuir adsorption model can be represented as under,

$$q_e = \frac{q_{max}bC_e}{1+bC_e} \dots\dots\dots (3)$$

Adsorption parameters were evaluated following the linear form of equation 3,

$$\frac{1}{q_e} = \frac{1}{q_{max}} + \left[ \frac{1}{q_{max}b} \right] \frac{1}{C_e} \dots\dots\dots (4)$$

Where, q<sub>max</sub> is the maximum monolayer capacity of adsorbent (mg/g), b is the Langmuir constant (L/mg), C<sub>e</sub> is the concentration of adsorbate under equilibrium conditions (mg/L) and q<sub>e</sub> is the amount of adsorbate per gram of adsorbent at equilibrium (mg/g).

The value of q<sub>max</sub> and b was obtained from the slope and intercept of the plot of 1/q<sub>e</sub> versus 1/C<sub>e</sub> as shown in Fig 1. The results of Langmuir plot are shown in Table 3.

An important characteristic of the Langmuir isotherm may be expressed in terms of dimensionless equilibrium parameter constant R<sub>L</sub> [17] expressed as,

$$R_L = \frac{1}{1+(1+bC_o)} \dots\dots\dots (5)$$

Where, C<sub>o</sub> is the initial adsorbate concentration and b is the Langmuir isotherm constant. According to Hameed et al., 2007, Bayramoglu et al., 2009 and Ghanizdeh et al., 2010, the value of R<sub>L</sub> gives a good approximation of adsorption characteristics, the nature of adsorption is unfavorable if R<sub>L</sub>>1, linear if R<sub>L</sub>=1, favorable if 0< R<sub>L</sub><1 and irreversible if R<sub>L</sub>=0. From the values computed in Table 3, it can be seen that the value of R<sub>L</sub> lies between 0 and 1 indicating that the adsorption experiment considering the Langmuir isotherm model is favorable under the specified experimental conditions of this research work. Also, from the

results it can be noted that the coefficient of regression value,  $R^2$  is 0.926 which signifies that the isotherm model gives good and best fit with the experimental adsorption data under specified experimental conditions.

**B. FREUNDLICH ADSORPTION ISOTHERM**

The Freundlich adsorption model normally applies for the heterogeneous surface. The isotherm model was plotted to study the intensity of adsorption of adsorbent for the adsorbate [21]. The linear form of Freundlich isotherm equation is expressed as,

$$\log q_e = \log K_f + \frac{1}{n} \log C_e \dots\dots\dots (6)$$

Where,  $K_f$  is the Freundlich isotherm constant signifies the capacity of adsorption process (mg/g), while  $n$  gives good approximation of the adsorption intensity. Equation 6 was plotted against  $\log q_e$  versus  $\log C_e$  as shown in Fig 2 to get the values of  $n$  and  $K_f$  from the slope and intercept respectively. The adsorption data shows a reasonable fit with Freundlich isotherm model with  $R^2$  value of 0.884. A favorable adsorption process is estimated when the value of  $n$  lies between one and ten [22]. From the calculated results, it can be seen that the value of  $n$  is 1.61 indicating a favorable adsorption process. On the other hand,  $1/n$  is anticipated as a function of the adsorption strength in the adsorption process [23]. Specifically, the linear least-squares method and the linearly transformed equations have been widely applied to correlate sorption data where  $1/n$  is a heterogeneity parameter, the smaller  $1/n$ , the greater the expected heterogeneity [16]. If value of  $1/n$  is below one it indicates a normal adsorption process, while  $1/n$  being above one indicates cooperative adsorption [24]. From Table 3, the value of  $1/n$  is 0.619 indicating a normal adsorption process. It can be seen from equation 6 that the amount of adsorption varies linearly with pressure until the specific saturation pressure is reached after that no further adsorption is possible and the system attains equilibrium.

**C. TEMPKIN ISOTHERM MODEL**

The Tempkin isotherm model represents a linear relationship between the amount of adsorbate per gram of adsorbent at equilibrium and  $\ln C_e$ . Moreover, the adsorption model assumes that the heat of adsorption of each molecule decreases linearly with the coverage capacity by ignoring the extremities of concentration [25, 26]. The adsorption model is represented by following linear equation [25],

$$q_e = B \ln A + B \ln C_e \dots\dots\dots (7)$$

$$B = \frac{RT}{b_T} \dots\dots\dots (8)$$

Where,  $A$  represents the equilibrium Tempkin isotherm binding constant (L/g),  $R$  is the universal gas constant (8.314 J/mol/K),  $b_T$  is Tempkin constant,  $T$  is room temperature in K and  $B$  is the constant of heat of adsorption which usually express the type of adsorption (J/mol).

The linear equation 7 was plotted against  $q_e$  versus  $\ln C_e$  to get the values of B and A as the slope and intercept respectively and the value of  $b_T$  was calculated from equation 8. Fig 3 shows scattered nature of the graph with  $R^2$  value as 0.678 indicating less fit of Tempkin isotherm with the experimental adsorption data. From Table 3, the value of heat of adsorption is 8.239 J/mol indicating a physical adsorption process.

D. DUBININ–RADUSHKEVICH ISOTHERM MODEL

The adsorption mechanism considering the distribution of Gaussian energy onto heterogeneous surface is normally represented by Dubinin–Radushkevich isotherm model [27]. The model is represented by linear equation 9.

$$\ln q_e = \ln q_s - (K_{ad} \varepsilon^2) \dots\dots\dots (9)$$

Where,  $q_s$  is termed as the theoretical value of isotherm adsorption capacity (mg/g),  $K_{ad}$  is Dubinin–Radushkevich isotherm constant ( $\text{mol}^2/\text{KJ}^2$ ) and  $\varepsilon$  is Dubinin–Radushkevich isotherm constant. The graph of  $\ln q_e$  versus  $\varepsilon^2$  considered as the DRK isotherm plot yields the value of logarithm of theoretical adsorption capacity  $\ln q_s$  as the intercept and DRK constant  $K_{ad}$  as the slope of the characteristics curve. The apparent energy of adsorption (E) which is a measure of the characteristics of adsorption process is calculated from equation 10.

$$E = \frac{1}{\sqrt{2B_{DR}}} \dots\dots\dots (10)$$

Where  $B_{DR}$  is expressed as the isotherm constant, whereas, the parameter  $\varepsilon$  can be calculated by the equation 11,

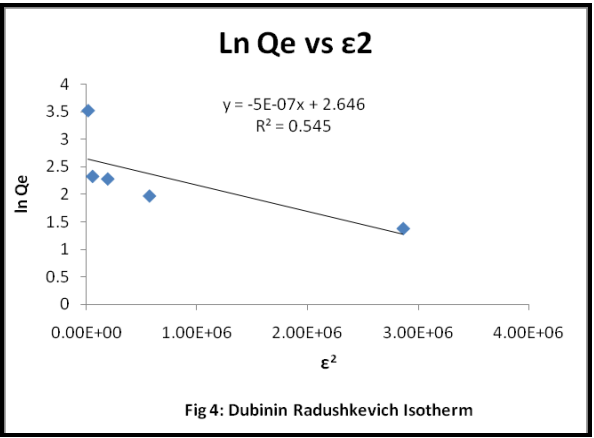
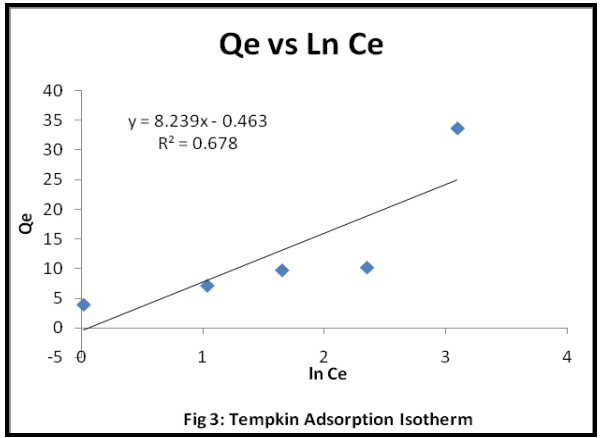
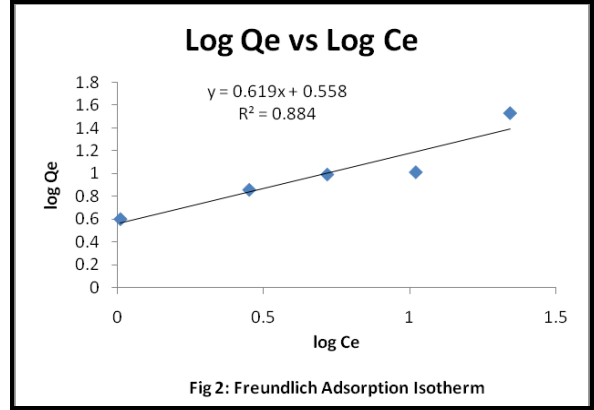
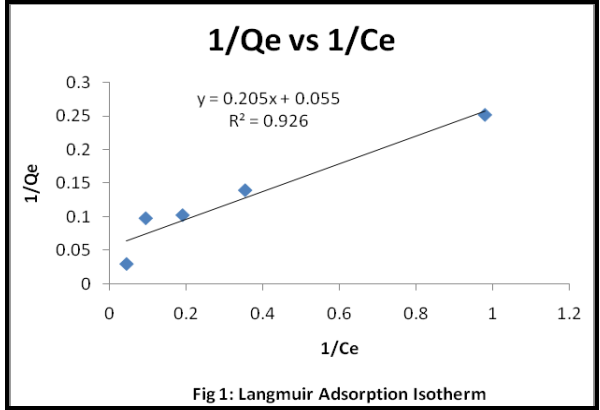
$$\varepsilon = RT \times \ln \left[ 1 + \frac{1}{C_e} \right] \dots\dots\dots (11)$$

Where, R is gas constant (8.314 J/mol K), T is the absolute temperature (K) and  $C_e$  is the adsorbate equilibrium concentration (mg/L). The DRK isotherm parameters are tabulated as per Table 3. As can be seen from Fig 4 this isotherm model also does not provide a good fit with the adsorption data and the  $R^2$  value is 0.545. P. Sivakumar et al. found that if the value of E lies between 8 and 16 kJ/mol then it indicates a chemisorptions process, whereas, if the value lies below 8 kJ/mol then it indicates a physical adsorption process. Here from the DRK plot the apparent energy of adsorption (E) value is obtained as 1 kJ/mol indicates physical adsorption process between unmodified eggshell and Fe(III) ions.

Table 2:- Parameters for plotting equilibrium Adsorption Isotherm Models of Fe(III) onto unmodified hen egg shell											
Sr. No.	$C_o$	$C_e$	$1/C_e$	$\log C_e$	$\ln C_e$	$Q_e$ (mg/g)	$1/Q_e$	$\log Q_e$	$\ln Q_e$	$C_e/Q_e$ (g/l)	$\varepsilon^2$
1	5	1.02	0.98039	0.0086	0.0198	3.98	0.25126	0.59988	1.38128	0.25628	$2.86 \times 10^6$
2	10	2.82	0.35461	0.45025	1.03674	7.18	0.13928	0.85612	1.9713	0.39276	$5.66 \times 10^5$
3	15	5.22	0.19157	0.71767	1.6525	9.78	0.10225	0.99034	2.28034	0.53374	$1.88 \times 10^5$
4	20	10.5	0.09524	1.02119	2.35138	10.24	0.09766	1.0103	2.3263	1.02539	$5.10 \times 10^4$
5	50	22.1	0.04525	1.34439	3.09558	33.7	0.02967	1.52763	3.5175	0.65579	$1.20 \times 10^4$

Table 3:- Langmuir, Freundlich, Temkin and Dubinin-Raduskevich isotherm constants for the adsorption of Fe(III) onto unmodified hen egg shell

Isotherm	Isotherm Constants			
	Langmuir	$Q_{max}$ (mg/g)	$b$ (L/mg)	$R_L$
18.18		0.268	0.136	0.93
Freundlich	$1/n$	$n$	$K_f$ (mg/g)	$R^2$
	0.619	1.61	3.61	0.88
Temkin	$A$ (L/mg)	$b_T$	$B$	$R^2$
	0.945		(J/mol)	
Dubinin-Radushkevich	$q_s$ (mg/g)	$K_{ad}$ (mol <sup>2</sup> /KJ <sup>2</sup> )	$E$ (KJ/mol)	$R^2$
	14.097	$0.5 \times 10^{-6}$	1	0.55



IV. CONCLUSION

The experimental result showed the use of unmodified hen eggshell as a low cost adsorbent for Fe(III) bearing aqueous solution. The adsorption isotherm observed in the range of Langmuir > Freundlich > Temkin > Dubinin–Radushkevich. Physical adsorption was confirmed with the apparent energy of adsorption (1.0 kJ/mol) in a Dubinin-Radushkevich isotherm and heat of adsorption (8.239 J/mol) from Tempkin isotherm model. Favourable adsorption was analyzed from separation factor ( $R_L=0.136$ ) in a Langmuir isotherm and cross verified by adsorption intensity ( $n=1.61$ ) in a Freundlich isotherm. Hence, hen egg shell can be utilised as a low cost bio waste sorbent for the removal of Fe(III) from aqueous solution without chemical treatment as this will increase the cost of application.



### ACKNOWLEDGMENT

The authors would like to thank professors and lab assistants of Chemical Engineering Department and Environmental Audit Cell of S. N. Patel Institute of Technology & Research Centre, Umrakh, Bardoli for their extended motivational and infrastructure support in carrying out this research work.

### REFERENCES

- [01] Asli Baysal, Nil Ozbek and Suleyman Akman, "Determination of Trace Metals in Waste Water and Their Removal Processes", Waste Water - Treatment Technologies and Recent Analytical Developments, 2013.
- [02] Iriany, Krisnawati and Jasinda, "Adsorption of Heavy Metal Iron Fe(III) using Activated Powdered Duck Eggshell Adsorbent", the 11<sup>th</sup> International Conference on mining, Materials and Petroleum Engineering, Thailand, Chiang Mai, November, 2013.
- [03] B. Subramanyam and A. Das, "Linearized and non-linearized isotherm models comparative study on adsorption of aqueous phenol solution in soil", Int. J. Environ. Sci. Tech., 6 (4), 2009, 633-640.
- [04] J. C. Igwe and A. A. Abia., "A bio-separation process for removing heavy metals from waste water using bio-sorbents", African Journal of Biotechnology, 5 (12), 2006, 167-1179.
- [05] N. T. Abdel-Ghani; Hefny, M. and G.A.F. El-Chagbawy, "Removal of Lead (II) from aqueous solution using low cost abundantly available adsorbents". Int. J. Environ. Sci. Tech., 4 (1), 2007, 67-73.
- [06] Nitin Verma, Vivek Kumar, Mukesh C. Bansal, "Utilization of Egg Shell Waste in Cellulase Production by Neurospora crassa under Wheat Bran-Based Solid State Fermentation", Pol. J. Environ. Stud. Vol. 21, No. 2 (2012), 491-497.
- [07] William, J. S. and J. C. Owen, Egg Science and Technology. 4<sup>th</sup> Ed., Food Product Press, New York, P: 950, 1995.
- [08] Dhuha D. Salman, Wisam S. Ulaiwi and N. M. Tariq, "Determination the Optimal Conditions of Methylene Blue Adsorption by the Chicken Egg Shell Membrane", International Journal of Poultry Science 11 (6): 391-396, 2012.
- [09] A. Nurlaela, Penambahan Kristal Apatit dari Cangkang Telur Ayam dan Bebek, IPB, 2009. Indonesian Language, 2009.
- [10] Darmono (2008), Kadmium (Cd) dalam lingkungan dan Pengaruhnya Terhadap Kesehatan dari Produktivitas Ternak, WARTAZOA, 2008, 8(1), hal. 28 – 32. Indonesian Language, 2008.
- [11] Ruswanti, Indah; Khabibi M.Si. dan Retno, Anadi Lusiana, M. Si (2009), Membran Kitosan Padat dari Cangkang Rajungan (*Portunus pelagicus*) dan Aplikasinya Sebagai Adsorben Ion Mangan (II) dan Besi (II), Universitas Diponegoro, Semarang, 2010. Indonesian Language, 2010.
- [12] G. W. Saer. "Determination of Specific surface area of sodium hydroxide". Anal. Chem. 28 (2), 1956, 1981 – 1983.
- [13] S. Toshiguki and K. Yukata, "Pyrolysis of Plant, Animal and Human Wastes"; Physical and Chemical Characterization of the Pyrolytic Product; Bioresource Technology, 90 (3), 2003, 241-247.

- [14] M. Vanderborght and E. Van Grieken (1977). Enrichment of trace metals in water by adsorption on activated carbon. *Anal. Chem* 49 (2): 311 – 316.
- [15] T. H. Vermeulan, K. R. Vermeulan and L. C. Hall. “Fundamental” *Ind. Eng. Chem.* 5 (1966), p212–223.
- [16] Dada, A. O, Olalekan, A. P, Olatunya, A. M, Dada, O, Langmuir, Freundlich, Temkin and Dubinin–Radushkevich Isotherms Studies of Equilibrium Sorption of  $Zn^{2+}$  Unto Phosphoric Acid Modified Rice Husk, *IOSR Int. J. of Applied Science*, Volume 3, Issue 1 (Nov. – Dec. 2012), PP 38-45.
- [17] T. N. Webber and R. K. Chakravarti: Pore and Solid Diffusion Models for fixed bed adsorbers. *J. Am. Inst. Chem. Eng.* 1974, 20: 228-238.
- [18] Hameed B.H., Din A.T.M., and Ahmad A.L., (2007). "Adsorption of methylene blue onto bamboo- based activated carbon: Kinetics and equilibrium studies". *Journal of Hazardous Materials* 141: 819-825.
- [19] Bayramoglu, G., Altintas, B., Arica, M.Y., (2009). "Adsorption kinetics and thermodynamic parameters of cationic dyes from aqueous solutions by using a new strong cation-exchange resin", *Chem. Eng. J.* 152 (2-3): 339- 346.
- [20] Ghanizadeh, Gh., Ehrampoush, M.H., Ghaneian, M.T., (2010). "Application of Iron Impregnated Activated Carbon for Removal of Arsenic from Water". *Iran. J. Environ. Health. Sci. Eng.* 7 (2): 145-156.
- [21] N. D. Hutson and R. T. Yang. ‘Adsorption. *J. Colloid Interf. Sci.* (2000), pp 189.
- [22] S. Goldberg. “Equations and Models Describing Adsorption Processes in Soils”. *Soil Science Society of America*, 677 S. Segoe Road, Madison, WI 53711, USA. *Chemical Processes in Soils. SSSA Book Series*, (2005) no. 8.
- [23] E. Voudrias, F. Fytianos and E. Bozani: Sorption Description isotherms of Dyes from aqueous solutions and Waste Waters with Different Sorbent materials, *Global Nest, The Int. J.* 2002 4 (1), 75-83.
- [24] S. Mohan and J. Karthikeyan. “Removal of lignin and tannin color from aqueous solution by adsorption on to activated carbon solution by adsorption on to activated charcoal”, *Environ. Pollut.* 97, (1997) pp.183-187.
- [25] M. I. Tempkin, V. Pyzhev, “Kinetics of ammonia synthesis on promoted iron catalyst”, *Acta Phys. Chim. USSR* 12 (1940), 327–356.
- [26] C. Aharoni, M. Ungarish, “Kinetics of activated chemisorptions”. Part 2. Theoretical models, *J. Chem. Soc. Faraday Trans.* 73 (1977) 456–464.
- [27] A. Gunay, E. Arslankaya, I. Tosun, “Lead removal from aqueous solution by natural and pretreated clinoptilolite: adsorption equilibrium and kinetics”, *J. Hazard. Mater.* 146 (2007) 362–371.
- [28] P. Sivakumar, and P. N. Palanisamy, “Adsorption studies of basic red 29 by a non conventional activated carbon prepared from *euphorbia antiquorum L*”, *Int. J. Chem. Tech. Res*, Vol.1, no 3, pp 502-510, 2009.